

(1) Given: Observations of the piezometric heads in three observation wells:

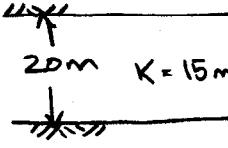
Well	A	B	C
x-coordinate	0	300 meters	0
y-coordinate	0	0	200 meters
Piezometric head (m)	+10.0 m	+11.5 m	+8.4 m

The wells penetrate a homogeneous, isotropic, confined aquifer of constant thickness $B=20$ meters, porosity = 0.2, and hydraulic conductivity $K = 15 \text{ m/day}$. Assume that the piezometric surface can be approximated as a plane.

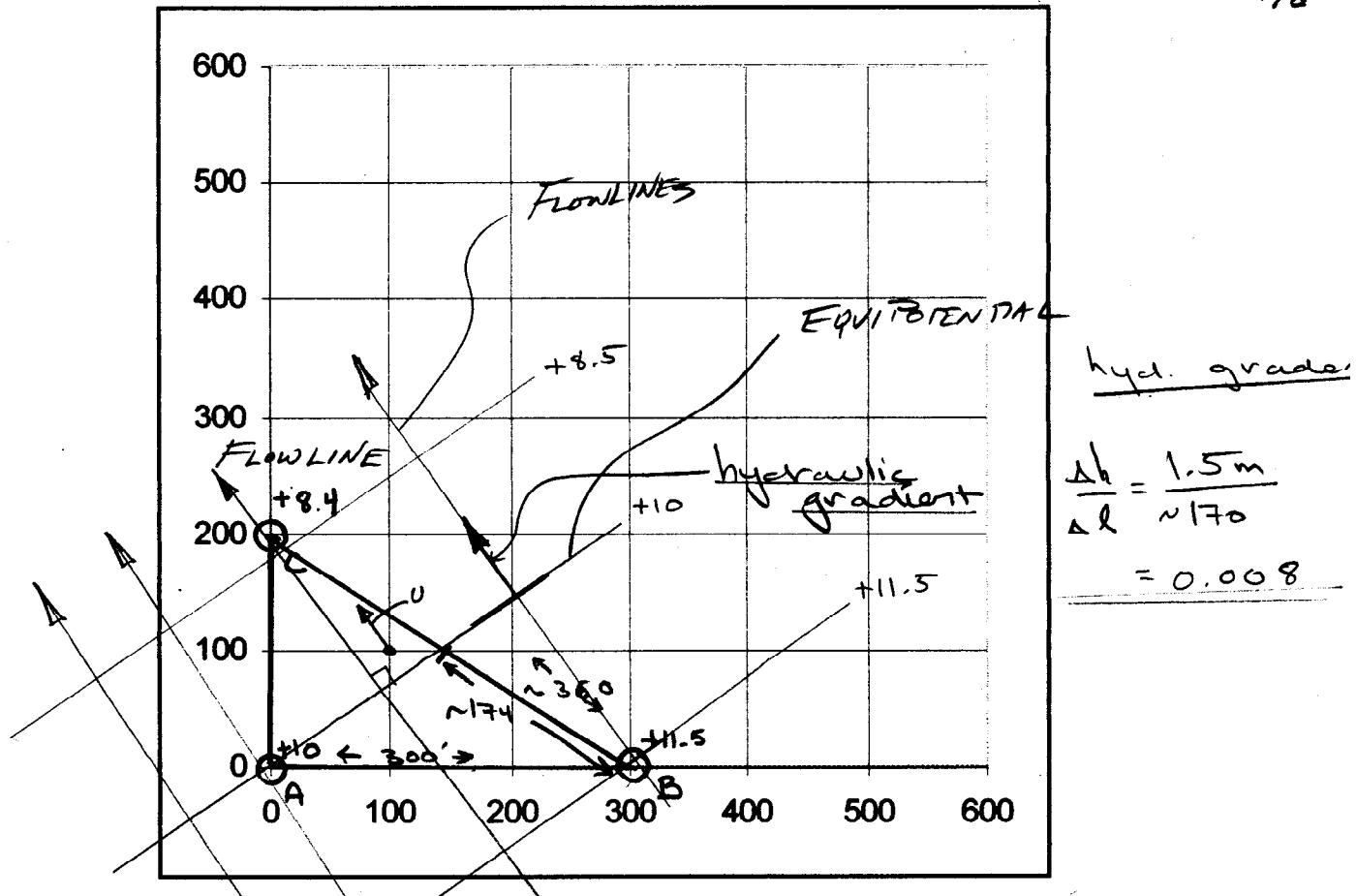
Determine:

- a) The hydraulic gradient (magnitude and direction)
- b) The aquifer transmissivity $T = 300 \text{ m}^2/\text{d}$
- c) The total discharge per unit width in the aquifer along a flow line
- d) The pore velocity at point P(100,100).
- e) Sketch the flowlines and equipotential lines for this aquifer.

Transmissivity



 $T = (K \cdot B) = (15 \text{ m/day}) \cdot (20 \text{ m}) = 300 \text{ m}^2/\text{d}$



$$\frac{11.5 - 8.4}{360} = \frac{11.5 - 10}{x}$$

Solve for x

$$x = \frac{(1.5) 360}{(3.1)} = 174$$

Problem 1 Worksheet.

$$Q = K \cdot A \frac{\Delta h}{\Delta L} = K \cdot B \cdot w \frac{\Delta h}{\Delta L}$$

$$\begin{aligned}\frac{Q}{B} &= \text{flow/width} = K \cdot B \frac{\Delta h}{\Delta L} \\ &= 300 \text{ m}^2/\Delta (0.008) \\ &= 2.64 \text{ m}^3/\Delta / \text{m}\end{aligned}$$

$$J_{\text{pure}} = \frac{K}{w} \frac{\Delta h}{\Delta L} = \frac{15 \text{ m}/\Delta}{0.20} \cdot 0.008 = 0.6 \text{ m}/\Delta$$

(2) Given: Same aquifer as problem 1. Aquifer dispersivities are $\alpha_L = 2.0 \text{ m}$, $\alpha_T = 0.2 \text{ m}$.

Determine:

- Longitudinal dispersion coefficient along a flowline.
- Transverse dispersion coefficient along a flowline.
- Distance along a flowline where the concentration from a reservoir-type source is reduced to 10% of its input concentration.

Table of Functions					
x	ERF(x)	ERFC(x)	x	ERF(x)	ERFC(x)
-3	-1.0000	2.0000	0	0.0000	1.0000
-2.9	-1.0000	2.0000	0.1	0.1125	0.8875
-2.8	-0.9999	1.9999	0.2	0.2227	0.7773
-2.7	-0.9999	1.9999	0.3	0.3286	0.6714
-2.6	-0.9998	1.9998	0.4	0.4284	0.5716
-2.5	-0.9996	1.9996	0.5	0.5205	0.4795
-2.4	-0.9993	1.9993	0.6	0.6039	0.3961
-2.3	-0.9989	1.9989	0.7	0.6778	0.3222
-2.2	-0.9981	1.9981	0.8	0.7421	0.2579
-2.1	-0.9970	1.9970	0.9	0.7969	0.2031
-2	-0.9953	1.9953	1	0.8427	0.1573
-1.9	-0.9928	1.9928	1.1	0.8802	0.1198
-1.8	-0.9891	1.9891	1.2	0.9103	0.0897
-1.7	-0.9838	1.9838	1.3	0.9340	0.0660
-1.6	-0.9763	1.9763	1.4	0.9523	0.0477
-1.5	-0.9661	1.9661	1.5	0.9661	0.0339
-1.4	-0.9523	1.9523	1.6	0.9763	0.0237
-1.3	-0.9340	1.9340	1.7	0.9838	0.0162
-1.2	-0.9103	1.9103	1.8	0.9891	0.0109
-1.1	-0.8802	1.8802	1.9	0.9928	0.0072
-1	-0.8427	1.8427	2	0.9953	0.0047
-0.9	-0.7969	1.7969	2.1	0.9970	0.0030
-0.8	-0.7421	1.7421	2.2	0.9981	0.0019
-0.7	-0.6778	1.6778	2.3	0.9989	0.0011
-0.6	-0.6039	1.6039	2.4	0.9993	0.0007
-0.5	-0.5205	1.5205	2.5	0.9996	0.0004
-0.4	-0.4284	1.4284	2.6	0.9998	0.0002
-0.3	-0.3286	1.3286	2.7	0.9999	0.0001
-0.2	-0.2227	1.2227	2.8	0.9999	0.0001
-0.1	-0.1125	1.1125	2.9	1.0000	0.0000
0	0.0000	1.0000	3	1.0000	0.0000

Problem 2 Worksheet

$$\begin{aligned} D_L &= \alpha_L V \\ &= (2.0 \text{ m})(0.6 \text{ m/d}) \\ &= 1.2 \text{ m}^2/\text{d} \end{aligned}$$

$$\begin{aligned} D_T &= \alpha_T V \\ &= (0.2 \text{ m})(0.6 \text{ m/d}) \\ &= 0.12 \text{ m}^2/\text{d} \end{aligned}$$

Constant reservoir

$$C(x, t) = \frac{C_0}{2} \left[\operatorname{erfc} \left(\frac{x-vt}{2\sqrt{D_L t}} \right) - \exp \left(\frac{xv}{D} \right) \underbrace{\operatorname{erfc} \left(\frac{x+vt}{2\sqrt{D_L t}} \right)}_{\text{negligible at } x > 10vt} \right]$$

Use

$$C(x, t) \approx \frac{C_0}{2} \operatorname{erfc} \left(\frac{x-vt}{2\sqrt{D_L t}} \right)$$

Find x for $C(x, t) = 0.1 C_0$

$$0.1 C_0 = \frac{C_0}{2} \operatorname{erfc} \left(\frac{x-vt}{2\sqrt{D_L t}} \right)$$

$$0.2 C_0 = C_0 \operatorname{erfc} \left(\frac{x-vt}{2\sqrt{D_L t}} \right)$$

$$0.2 = \operatorname{erfc} \left(\frac{x-vt}{2\sqrt{D_L t}} \right)$$

From table

$$\frac{x-vt}{2\sqrt{D_L t}} = 0.9$$

$$x = 1.8\sqrt{D_L t} + vt$$

(3) Given: Confined aquifer system depicted in figure P-4. Water enters the confined aquifer in the recharge area and leaves in the form of a spring.

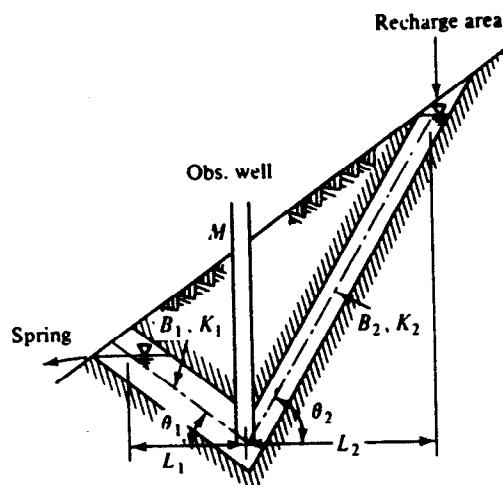


Figure P-4.

Determine:

- Piezometric head at a well located at M (in terms of the other variables)
- Specify the conditions for the well to become a flowing well (water flows from well without pumping)

Diagrams and equations for determining piezometric head and well conditions:

Left diagram: A right-angled triangle with vertical leg L_1 and horizontal leg d_1 . The hypotenuse is labeled h_1 .

$$\Delta h_1 = L_1 \sqrt{\tan^2 \theta_1 + 1}$$

$$h_1 = L_1 \tan \theta_1$$

Middle diagram: A right-angled triangle with vertical leg L_2 and horizontal leg d_2 . The hypotenuse is labeled h_2 .

$$\Delta h_2 = L_2 \sqrt{\tan^2 \theta_2 + 1}$$

Right side:

$$\Delta h_2 = \sqrt{L_2^2 + L_2^2 \tan^2 \theta_2}$$

$$= L_2 \sqrt{\tan^2 \theta_2 + 1}$$

Problem 3 Worksheet

$$Q_2 = K_2 B_2 \frac{\Delta h}{\Delta L} = K_2 B_2 \frac{L_2 \tan \theta_2 - h_m}{L_2 \sqrt{\tan^2 \theta_2 + 1}}$$

$$Q_1 = K_1 B_1 \frac{\Delta h}{\Delta L} = K_1 B_1 \frac{h_m - L_1 \tan \theta_1}{L_1 \sqrt{\tan^2 \theta_1 + 1}}$$

By continuity

$$Q = Q_1 = Q_2$$

$$\therefore K_1 B_1 \frac{h_m - L_1 \tan \theta_1}{L_1 \sqrt{\tan^2 \theta_1 + 1}} = K_2 B_2 \frac{L_2 \tan \theta_2 - h_m}{L_2 \sqrt{\tan^2 \theta_2 + 1}} \quad \text{Solve for } h_m$$

$$\frac{h_m - L_1 \tan \theta_1}{L_1 \sqrt{\tan^2 \theta_1 + 1}} = \frac{K_2 B_2}{K_1 B_1} \frac{L_2 \tan \theta_2 - h_m}{L_2 \sqrt{\tan^2 \theta_2 + 1}}$$

$$\frac{h_m}{L_1 \sqrt{\tan^2 \theta_1 + 1}} = \frac{K_2 B_2}{K_1 B_1} \frac{L_2 \tan \theta_2}{L_2 \sqrt{\tan^2 \theta_2 + 1}} - \frac{K_2 B_2 h_m}{K_1 B_1 L_2 \sqrt{\tan^2 \theta_2 + 1}} + \frac{L_1 \tan \theta_1}{L_1 \sqrt{\tan^2 \theta_1 + 1}}$$

$$\frac{h_m}{L_1 \sqrt{\tan^2 \theta_1 + 1}} + \frac{K_2 B_2 h_m}{K_1 B_1 L_2 \sqrt{\tan^2 \theta_2 + 1}} = \underbrace{\frac{K_2 B_2}{K_1 B_1} \frac{L_2 \tan \theta_2}{L_2 \sqrt{\tan^2 \theta_2 + 1}} + \frac{L_1 \tan \theta_1}{L_1 \sqrt{\tan^2 \theta_1 + 1}}}_{R}$$

$$\frac{h_m K_1 B_1 L_2 \sqrt{\tan^2 \theta_2 + 1} + h_m K_2 B_2 L_1 \sqrt{\tan^2 \theta_1 + 1}}{K_1 B_1 L_1 L_2 \sqrt{\tan^2 \theta_1 + 1} \sqrt{\tan^2 \theta_2 + 1}} = R$$

$$h_m = \left(\frac{K_1 B_1 L_1 L_2 \sqrt{\tan^2 \theta_2 + 1} \sqrt{\tan^2 \theta_1 + 1}}{K_1 B_1 L_2 \sqrt{\tan^2 \theta_2 + 1} + K_2 B_2 L_1 \sqrt{\tan^2 \theta_1 + 1}} \right) \left(\frac{K_2 B_2 L_2 \tan \theta_2 + L_1 \tan \theta_1}{K_1 B_1 L_2 \sqrt{\tan^2 \theta_2 + 1}} \right) \frac{L_1 \sqrt{\tan^2 \theta_1 + 1}}{L_1 \sqrt{\tan^2 \theta_2 + 1}}$$

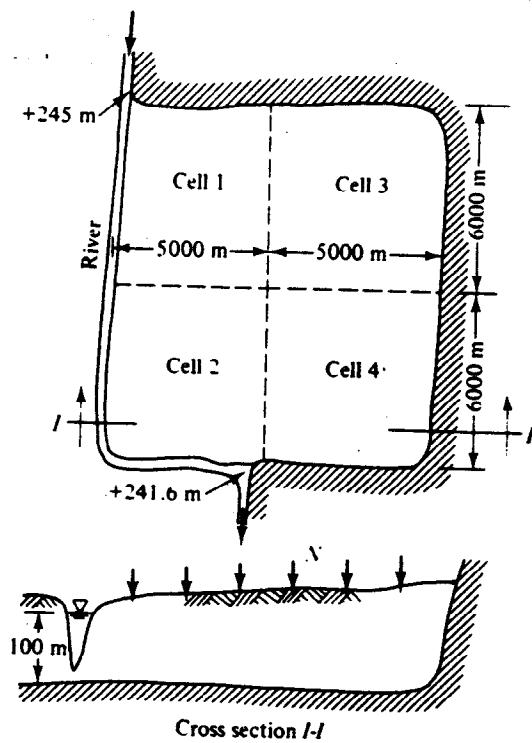
$$h_m = \frac{K_2 B_2 L_1 L_2 \sqrt{\tan^2 \theta_2 + 1} \tan \theta_2 + K_1 B_1 L_1 L_2 \sqrt{\tan^2 \theta_2 + 1} \tan \theta_1}{K_2 B_2 L_1 L_2 \sqrt{\tan^2 \theta_2 + 1} \tan \theta_2 + K_1 B_1 L_1 L_2 \sqrt{\tan^2 \theta_2 + 1} \tan \theta_1} \quad \leftarrow (a)$$

$$\frac{h_2 - h_1}{L_2 + L_1} = \text{slope of land.}$$

$$\left(\frac{L_2 \tan \theta_2 - L_1 \tan \theta_1}{L_2 + L_1} \right) \cdot L_1 + L_1 \tan \theta_1 < h_m$$

then
well will
flow!

- (4) Given: A four-cell conceptual model of an aquifer with the following cell-by-cell data summary.



$R = \text{mn/yr} * 1000 * 5000 * 6000$

Pumping ($10^6 \text{ m}^3/\text{yr}$)	Nat. replenishment (mm/yr)	$R (10^6 \text{ m}^3/\text{yr})$	$R = \text{mn/yr} * 1000 * 5000 * 6000$
Cell 1 17.8	200	6.0	40
Cell 2 0	420	12.6	40
Cell 3 6.3	300	9.0	30
Cell 4 2.7	300	9.0	30
Σ	26.8	36.6	

Determine:

- a) Write the governing steady-state balance equations that must be solved to calculate the steady average water levels in the four cells.
- b) Without actually solving these equations determine if the aquifer is a net supplier of water to the river or if the aquifer draws water from the river. (Show how you arrived at your answer).

Problem 4 Worksheet

a) Cell #1 $\delta = P_1 - R_1 + \frac{K_1 h_1 + K_3 h_3}{2} \left[\frac{h_3 - 2h_1 + h_R}{\Delta x^2} \right]$

$$+ \frac{K_1 h_1 + K_2 h_2}{2} \left[\frac{h_2 - 2h_1 + h_1}{\Delta y^2} \right]$$

Cell #2 $\delta = P_2 - R_2 + \frac{K_2 h_2 + K_4 h_4}{2} \left[\frac{h_4 - 2h_2 + h_R}{\Delta x^2} \right]$

$$+ \frac{K_2 h_2 + K_1 h_1}{2} \left[\frac{h_R - 2h_2 + h_2}{\Delta y^2} \right]$$

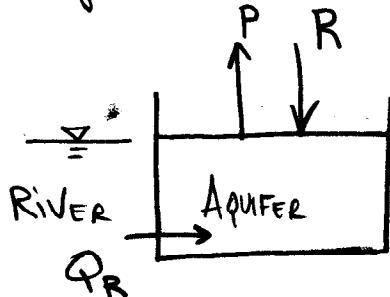
Cell #3 $\delta = P_3 - R_3 + \frac{K_3 h_3 + K_1 h_1}{2} \left[\frac{h_3 - 2h_3 + h_1}{\Delta x^2} \right]$

$$+ \frac{K_3 h_3 + K_4 h_4}{2} \left[\frac{h_3 - 2h_3 + h_4}{\Delta y^2} \right]$$

Cell #4 $\delta = P_4 - R_4 + \frac{K_4 h_4 + K_2 h_2}{2} \left[\frac{h_4 - 2h_4 + h_2}{\Delta x^2} \right]$

$$+ \frac{K_4 h_4 + K_3 h_3}{2} \left[\frac{h_3 - 2h_4 + h_4}{\Delta y^2} \right]$$

b) Water Budget entire aquifer



$$\delta = R - P + Q_R$$

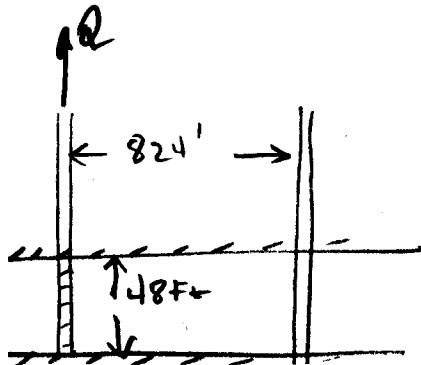
$$\begin{aligned} Q_R &= P - R \\ &= 26.8 - 36.6 \\ &= -9.8 \end{aligned}$$

∴ AQUIFER IS NET SUPPLIER
TO RIVER

(5) Given: Corrected time-drawdown data for a pumping test in a confined aquifer pumped at 42,400 cubic feet per day. The aquifer is 48 feet thick. The observation well is 824 feet from the pumping well.

Determine:

- Sketch the pumping well and observation well conceptual model.
- Find the aquifer transmissivity and storage coefficient using Jacob's method.



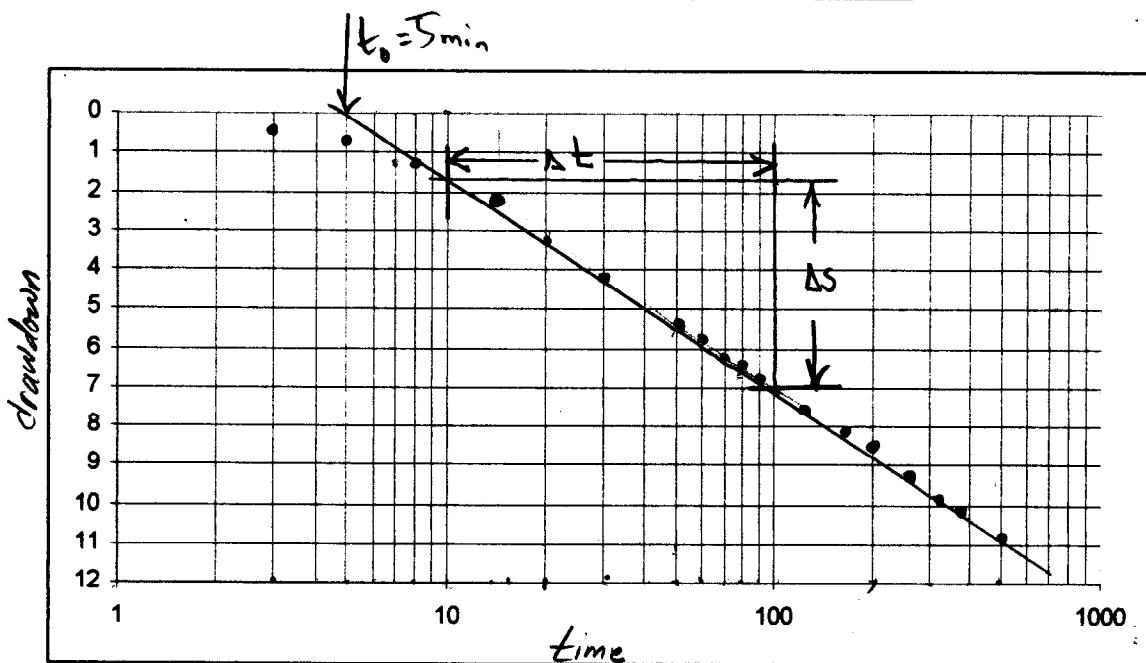
Time after pumping started (min)	Drawdown (feet)
3	0.3
5	0.7
8	1.3
12	2.1
20	3.2
24	3.6
30	4.1
38	4.7
47	5.1
50	5.3
60	5.7
70	6.1
80	6.3
90	6.7
100	7.0
130	7.5
160	8.3
200	8.5
260	9.2
320	9.7
380	10.2
500	10.9

- Convert Q
to ft^3/min

$$T_0 = 824 \text{ ft}$$

$$42400 \text{ ft}^3/\text{day} \cdot \frac{1 \text{ day}}{1440 \text{ min}}$$

$$29.4 \text{ ft}^3/\text{min}$$



$$t_2 = 100 \quad \Delta s = 5.2 \text{ ft}$$

$$t_1 = 10$$

Problem 5 Worksheet

$$T = \frac{Q}{4\pi \Delta S} \ln\left(\frac{t_2}{t_1}\right)$$

$$S = \frac{2.25 T}{r^2} t_0$$

$$T = \frac{29.4 \text{ ft}^3/\text{min}}{4\pi (5.2 \text{ ft})} \ln(10) = 1.03 \text{ ft}^2/\text{min}$$

$$S = \frac{2.25 (1.03)^2 (5 \text{ min})}{(824 \text{ ft})^2} = 0.000017$$