



# Fundamentals of Engineering Spring 2005 Review

## *Mechanics of Materials*

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## problem distribution

- morning: 7% (8 out of 120 problems)
- afternoon: 8% (5 out of 60 problems)

## subject areas

- 30% shear and bending stress (4) ✓
- 23% shear & bending diagrams (3) ✓
- 23% principal stresses (3) ✓
- 8% axial stress and strain (1) ✓
- 8% buckling (1) *last*
- 8% thermal stress (1) ✓

stress - has units of pressure  
(solids pressure)

strain - axial stress and strain  
normalized deformation

deformation  $\propto$  solids pressure

if linear, the elastic modulus is const. of paper.

stress  $\sigma = \frac{F}{A_0}$

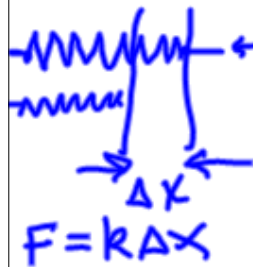
force

area

strain  $\epsilon = \frac{\Delta L}{L_0}$   $\epsilon_r = \frac{\Delta R}{R_0}$

change in length

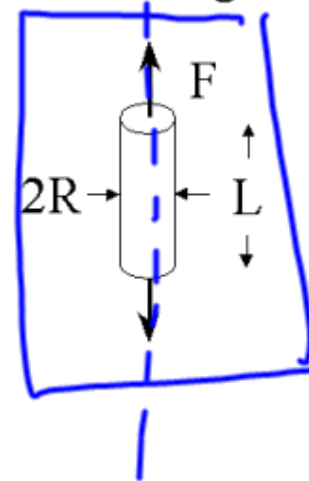
initial length



$F = k \Delta x$

elastic modulus  $E = \frac{\sigma}{\epsilon}$

Poisson's ratio  $\nu = -\frac{\epsilon_r}{\epsilon}$



2 ← used 2 in. diameter in "numbers" below.  $10 \cdot 10^6$  psi (Table)

A  $\frac{1}{2}$  in. diameter aluminum rod becomes 0.007 in. longer due to 1500 lbf tensile load. What is the rod's initial length and change in radius?



$$\epsilon = \frac{\Delta L}{L_0} \quad \epsilon_r = \frac{\Delta R}{R_0}$$

$$\Delta L = \epsilon L_0$$

$$L_0 = \frac{\Delta L}{\epsilon}$$

$$L_0 = \frac{0.007 \text{ in}}{4.77 \cdot 10^{-5}} = 146 \text{ in}$$

$$\Delta R = -\frac{\epsilon_r}{\epsilon} \cdot \epsilon \cdot R_0$$

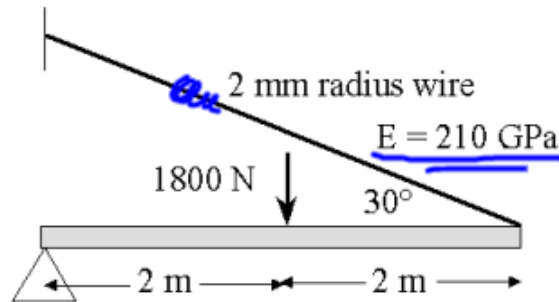
$$= -0.33 (4.77 \cdot 10^{-5}) \text{ in} = -1.57 \cdot 10^{-5} \text{ in}$$

$$E = \frac{\sigma}{\epsilon} = \frac{F}{\pi R_0^2 \epsilon}$$

$$[\nu = 0.33 \text{ (Table)}]$$

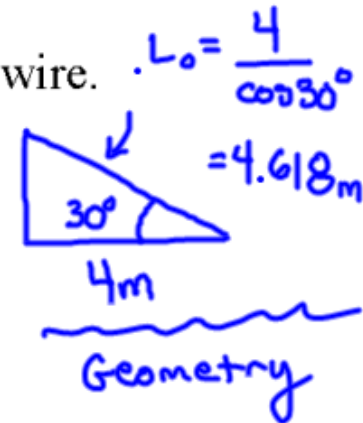
$$\epsilon = \frac{F}{\pi R^2 E} = \frac{1500 \text{ lb}}{\pi (1 \text{ in})^2 (10 \cdot 10^6 \frac{\text{lb}}{\text{in}^2})} = 4.77 \cdot 10^{-5}$$

33. Determine the change in length of the steel wire.

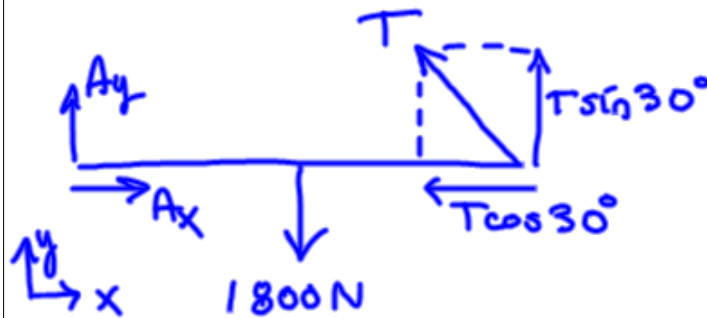


$E = 210 \text{ GPa}$

$210 \cdot 10^9 \text{ Pa}$



① FBD



② Find forces

$$\sum M_A = -1800(2) + T \sin 30^\circ(4)$$

$$T = \frac{1800(2)}{\sin 30^\circ(4)} = 1800 \text{ N}$$

$$\begin{aligned} \textcircled{3} \quad \underline{\Delta L} &= L_0 \epsilon = L_0 \frac{\sigma}{E} = \frac{L_0 T}{E A_0} = \frac{(4.618 \text{ m})(1800 \text{ N})}{210 \cdot 10^9 \frac{\text{N}}{\text{m}^2} \pi (0.002 \text{ m})^2} \\ &= 3.149 \cdot 10^{-3} \text{ m} \end{aligned}$$

materials expand/contract with  $\Delta T$  temp.  
- deformation is thermal strain.  
- if free to deform, then no stress

### thermal strain

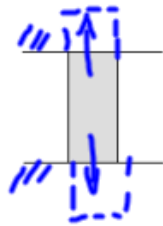
change in temperature

$$\varepsilon_T = \alpha \underbrace{(T - T_0)}_{\text{change in temperature}} \quad \left. \vphantom{\varepsilon_T} \right\} \text{linear driving force model}$$

coefficient of thermal expansion

$$\text{change in length} \quad \delta_T = \alpha L \underbrace{(T - T_0)}_{\Delta T} \quad \left. \vphantom{\delta_T} \right\}$$

101. A steel rod ( $E = 210 \text{ GPa}$ ,  $\alpha = 11.7 \times 10^{-6} \text{ }^\circ\text{C}^{-1}$ ) is constrained and heated. What is the stress induced by a  $40^\circ\text{C}$  increase in temperature?



① Virtual work  
② Combined

① Virtual work

(i) let expand

$$\Delta L = \alpha L_0 (T - T_0)$$

$$\frac{\Delta L}{L_0} = \epsilon_T = \alpha (T - T_0)$$

(ii) Apply axial stress equivalent to the thermal deformation

$$\epsilon_T E = \sigma = \frac{F}{A_0}$$

$$\begin{aligned} \sigma &= \alpha (T - T_0) E = (11.7 \cdot 10^{-6} / ^\circ\text{C}) (40^\circ) (210 \cdot 10^9 \frac{\text{N}}{\text{m}^2}) \\ &= 98.2 \cdot 10^3 \text{ kN/m}^2 = 98.2 \cdot 10^3 \text{ kPa} \\ &= 98.2 \cdot 10^6 \text{ Pa} \end{aligned}$$

Beams internal effects  
resisting

bending  
shear  
torsion

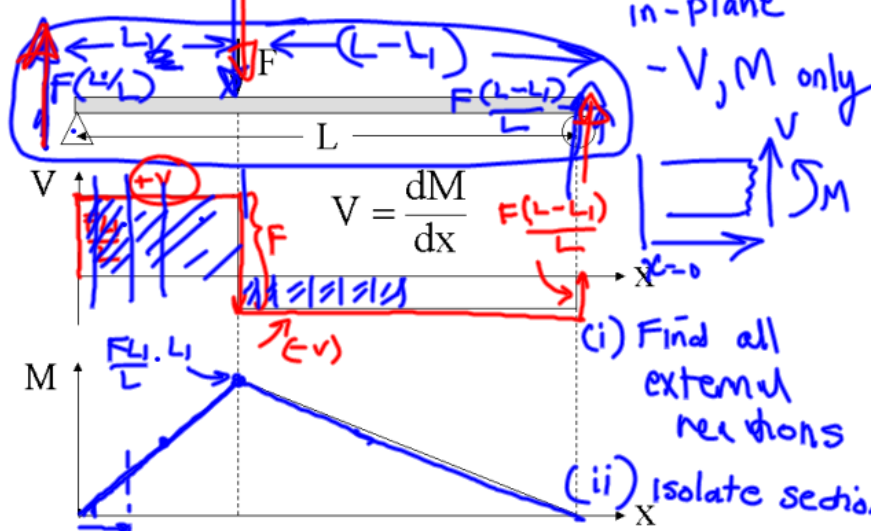
bending

shear

torsion

action/reaction

### shear and bending diagrams



$V, M, T$  be equal & opposite at internal surface

(v) distributed loads  
 $\frac{d}{dx} \left( \frac{dM}{dx} \right) = -w(x)$

$$\frac{dM}{dx} = V = \int -w(x) dx$$

$$= -w(x) \cdot x + C$$

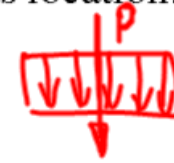
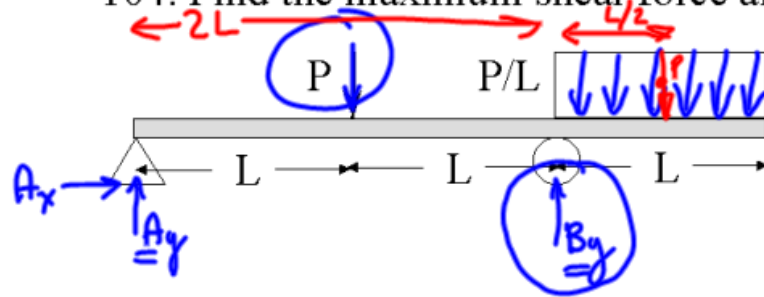
$$M = \int V dx = -\frac{w(x)x^2}{2} + Cx + D$$

is  $V, M$

- (i) Find all external reactions
- (ii) Isolate section equilibrium  $V \& M$
- (iii) Move section & try to find  $V \& M$  at new location
- (iv) Point loads & couples  $\Rightarrow$  discontinuous change



104. Find the maximum shear force and its location.

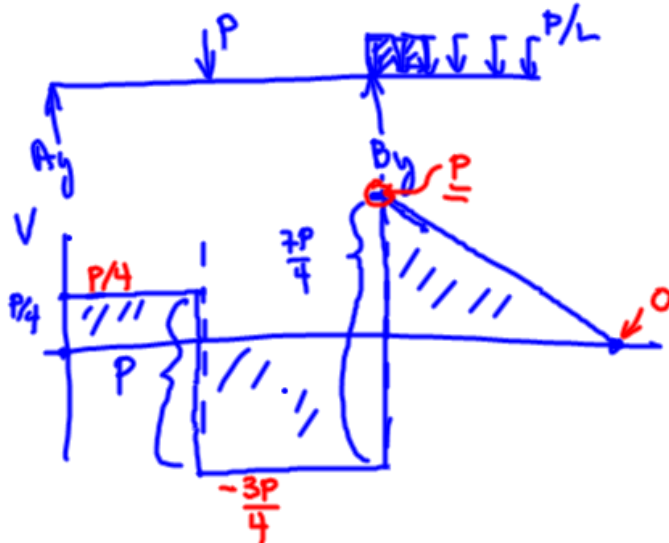


$$\sum M_A = 0 = -PL + 2B_y L - P \frac{5L}{2}$$

$$B_y = \frac{\frac{2PL}{2} + \frac{5PL}{2}}{2L} = \frac{7P}{4}$$

$$\sum F_y = 0 = A_y - 2P + B_y$$

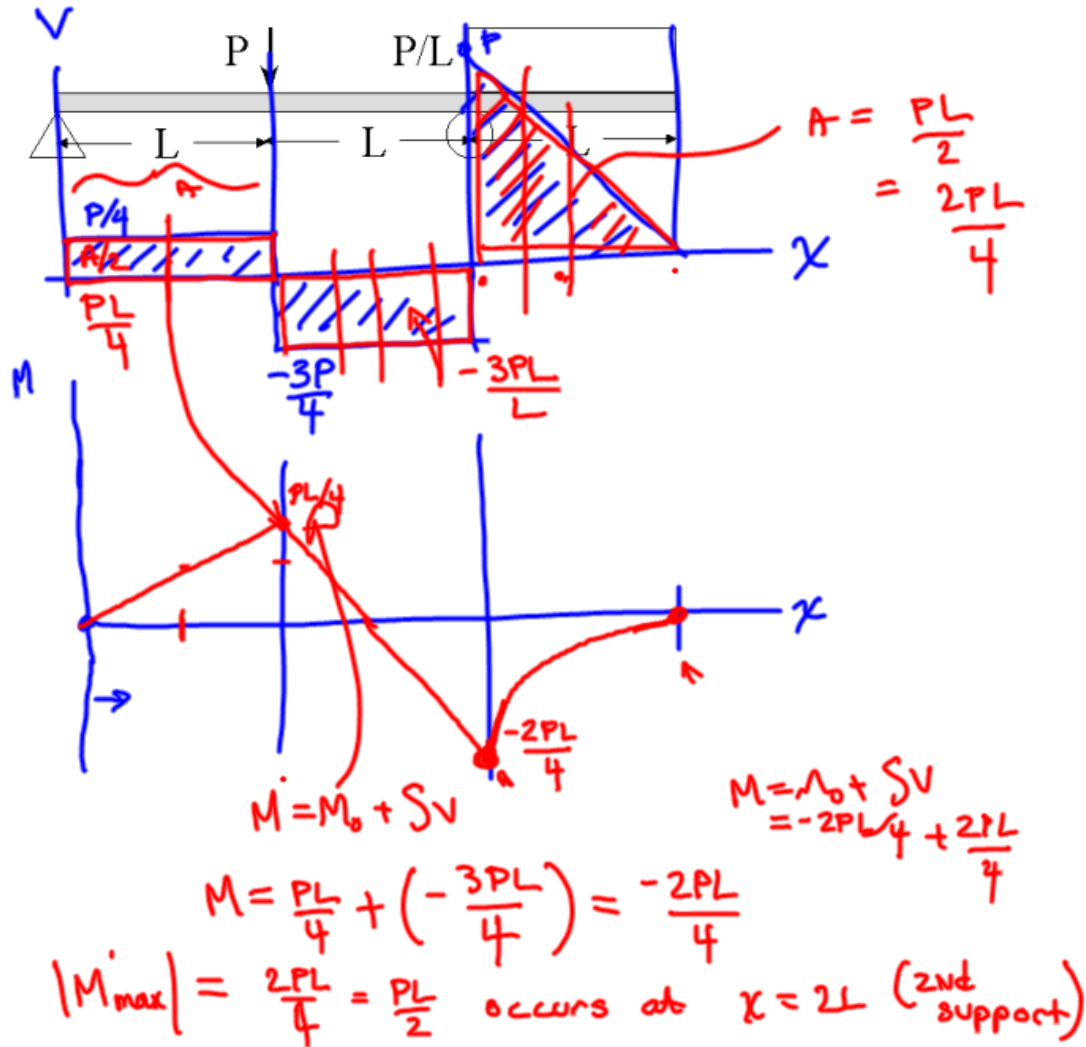
$$A_y = 2P - \frac{7P}{4} = \frac{P}{4}$$



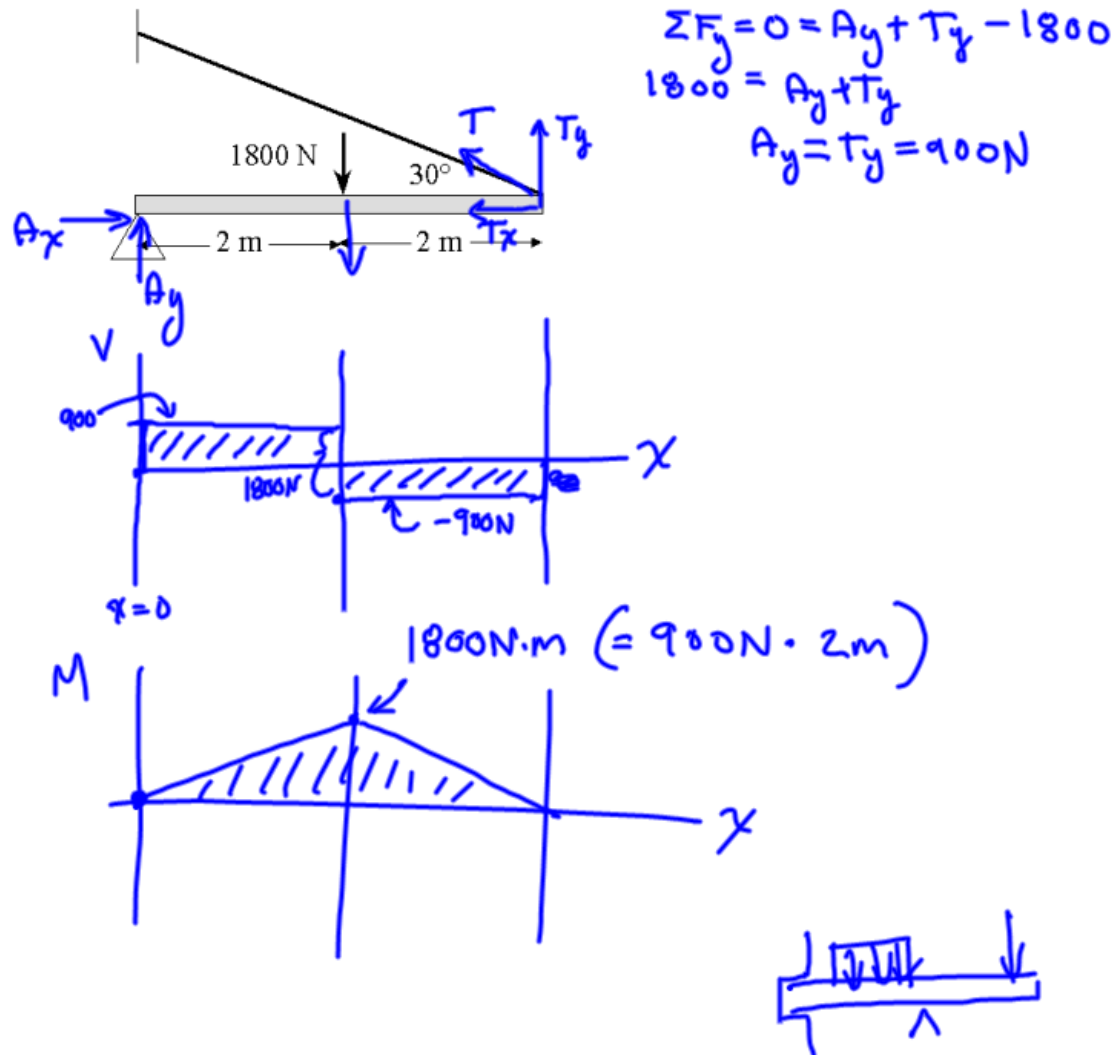
$$v = v_0 - \int w(x) dx$$

$V = P$   
 $V_{max}$   
 located at  $x = 2L$   
 (2<sup>ND</sup> support)

105. Find the maximum bending moment.



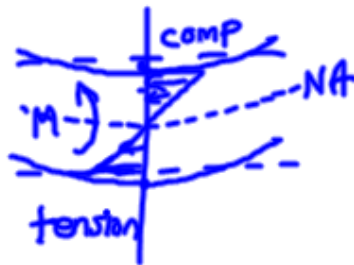
37. Sketch the shear and bending moment diagrams.



internal stress  
in beam ~~section~~  
section

relative to  
neutral axis

## bending stress



bending  
formula

bending moment

$$\sigma = -\frac{My}{I}$$

\* ← position

changes with  
section geometry



2nd moment of area

- "y" is measured from the neutral surface (centroid)
- "I" is calculated about the neutral surface (centroid)

$$I = I_c + Ad^2$$

↙ distance from N.A. to centroid, I<sub>c</sub>

34. Determine the maximum bending stress.

will occur where  $M$  is max.

$\sigma = -\frac{My}{I}$  ← geometric

load →  $I$  ← geometric

cross section

1800 N

30°

2 m

2 m

2 cm

6 cm

N.A.

3 cm

$$I_c = \frac{bh^3}{12}$$

$$= \frac{2(6)^3}{12} = \frac{1}{6} \cdot 6^3 = 36 \text{ cm}^4$$

$$\sigma(y) = -\frac{1800 \text{ N} \cdot \text{m} \cdot y}{36 \text{ cm}^4}$$

$$= -\frac{1800 \text{ N} \cdot 100 \text{ cm} \cdot y}{36 \text{ cm}^4}$$

$$= -\frac{1800 \text{ N} \cdot 100 \text{ cm} \cdot (3 \text{ cm})}{36 \text{ cm}^4}$$

$$= -\frac{6 \cdot 6 \cdot 100 \text{ N} \cdot 100 \text{ cm} \cdot 3 \text{ cm}}{2 \cdot 6 \cdot 6 \text{ cm}^4}$$

$$= \frac{30,000 \text{ N cm}^2}{2 \text{ cm}^4}$$

$$= \frac{15,000 \text{ N}}{\text{cm}^2}$$

↑  
convert to "m"

shear stress  
~~is~~ integral  
of bending  
stress

$$\tau_x(y) = \int \sigma_x(y) dy$$

shear stress

$\bar{y}A$  (~~cent~~  
area  
above  
N.A.)

shear force

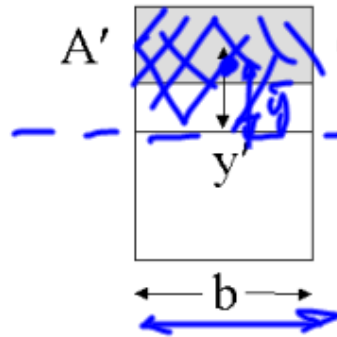
shear  
formula

$$\tau = \frac{VQ}{Ib}$$

← 1<sup>st</sup> moment  
of area

2nd moment of area

$$\tau = \frac{V \cdot \bar{y}A}{I b}$$



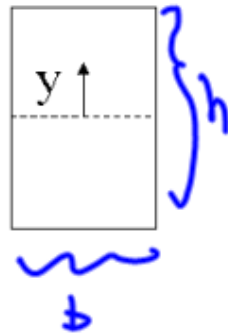
$$Q = \bar{y}'A'$$

N.A.

composite

$$I = I_c + Ad^2$$

102. What is the largest shear stress in a beam with a rectangular cross section?



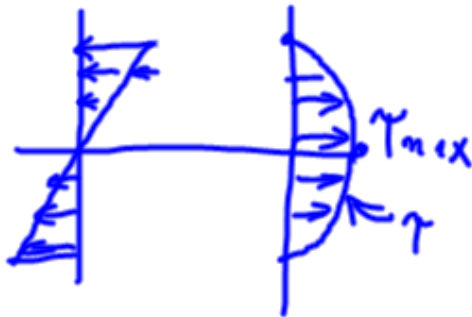
$$\tau = \frac{VQ}{Ib}$$

$$Q = \frac{h}{2} \cdot \frac{bh}{2} = \frac{bh^2}{4}$$

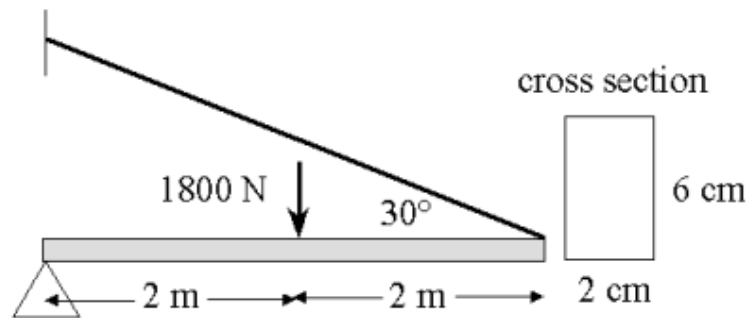
$$I = \frac{bh^3}{12} \quad \leftarrow \text{Table}$$

$$\tau = \frac{V \frac{bh^2}{8}}{\frac{bh^3}{12} \cdot b}$$

$$= \frac{3}{2} \frac{V}{bh}$$



35. Determine the maximum shear stress.



$$\tau = \frac{VQ}{Ib}$$

Handwritten annotations: "load" with an arrow pointing to V, and "geometric" with arrows pointing to Q, I, and b.

$\tau_{max}$  occurs at  $V_{max}$



$$\begin{aligned} \tau &= \frac{3}{2} \frac{V}{bh} \\ &= \frac{3}{2} \frac{900\text{N}}{(0.02\text{m})(0.06\text{m})} \\ &= 1.125 \cdot 10^6 \text{ N/m}^2 \\ &= 1.125 \text{ MPa} \end{aligned}$$



103. What is the ratio of maximum bending stress to the maximum shear stress in a cantilever beam with an end load and a rectangular cross section?

$\tau_{1/2} = ?$   
 $A_y = F \quad (\Sigma F_y = 0)$   
 $M_x = -FL$   
 Reactions

$$\sigma = -\frac{My}{I} = -\frac{(-FL)h/2}{\frac{bh^3}{12}} = \frac{6FL}{bh^2}$$

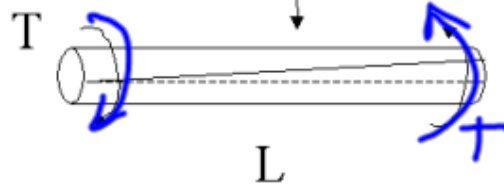
$$\tau = \frac{VQ}{Ib} = \frac{F \left( \frac{h}{4} \right) \left( \frac{bh}{2} \right)}{\frac{bh^3}{12} \cdot b} = \frac{F}{8bh}$$

$\tau_{1/2} = \frac{6FL}{bh^2} \cdot \frac{8bh}{12} = \frac{48}{12} \frac{L}{h} = \frac{4L}{h}$

$\bar{y}A = \left( \frac{h}{4} \right) \left( \frac{bh}{2} \right)$

# torsion

shear modulus  $G = \frac{\tau}{\gamma} = \frac{E}{2(1+\nu)}$



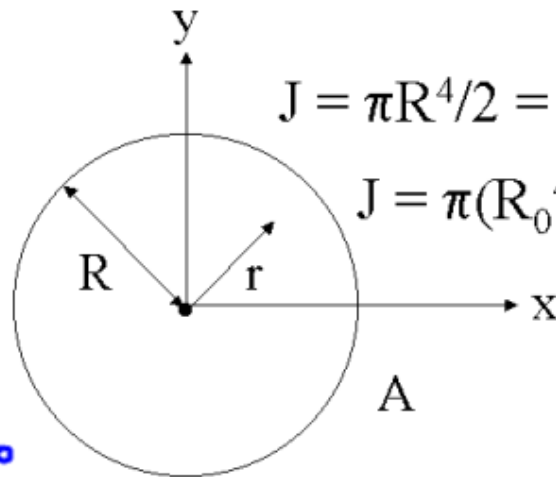
torsion formula  $\tau = \frac{Tr}{J}$  ← polar moment of area

angle of twist  $\phi = \frac{TL}{JG}$  ← material property

Moment of Inertia  
in polar  
coordinates

## polar moment of area

$$\underline{J = \int r^2 dA = \int (x^2 + y^2) dA = I_x + I_y}$$



$$J = \pi R^4 / 2 = \pi D^4 / 32 \text{ (solid)}$$

$$J = \pi (R_o^4 - R_i^4) / 2 \text{ (tube)}$$

10.16 A 10 cm diameter shaft can tolerate up to a 140 MPa shear stress. What is the maximum torque ( $\text{N}\cdot\text{m}$ )?

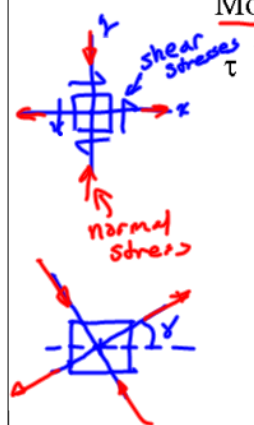
$$\begin{aligned}\tau &= \frac{T}{J}r \\ \tau &\leq 140 \text{ MPa} \\ T &= \frac{\tau J}{r} = \frac{(140 \cdot 10^6 \text{ Pa})(\pi D^4/32)}{0.05 \text{ m}} \\ &= 140 \cdot 10^6 \frac{\text{N}}{\text{m}^2} \cdot \frac{\pi (0.1)^4}{32 (0.05)} = 2.75 \cdot 10^4 \text{ N}\cdot\text{m}\end{aligned}$$

# principal stresses

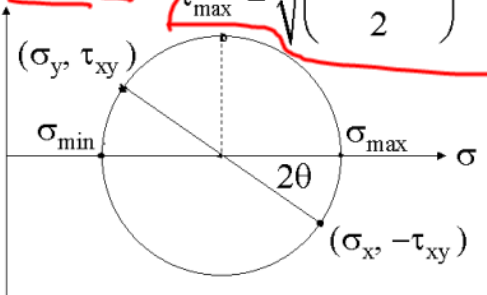
combined stresses  
bending  
torsion  
axial load

$$\sigma_{\max/\min} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\tau_{\max} = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$



Mohr's circle



plot on  $\tau, \sigma$  plane  
 $(\sigma_y, \tau_{xy})$   
 $(\sigma_x, -\tau_{xy})$   
 "draw circle that contains the two points"  
 - radius of that circle  
 $\tau_{\max}, \sigma_{\max}, \sigma_{\min}$   
 by inspection

100. Determine the maximum shear and normal stresses given  $\underline{\underline{\sigma_x}} = 6 \text{ MPa}$ ,  $\underline{\underline{\sigma_y}} = 0$  and  $\underline{\underline{\tau_{xy}}} = 4 \text{ MPa}$ .

$$\sigma_{\max} = \frac{\sigma_x + \sigma_y}{2} + \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$= \frac{6 + 0}{2} + \sqrt{\left(\frac{6}{2}\right)^2 + 4^2} = 3 + 5 = 8$$

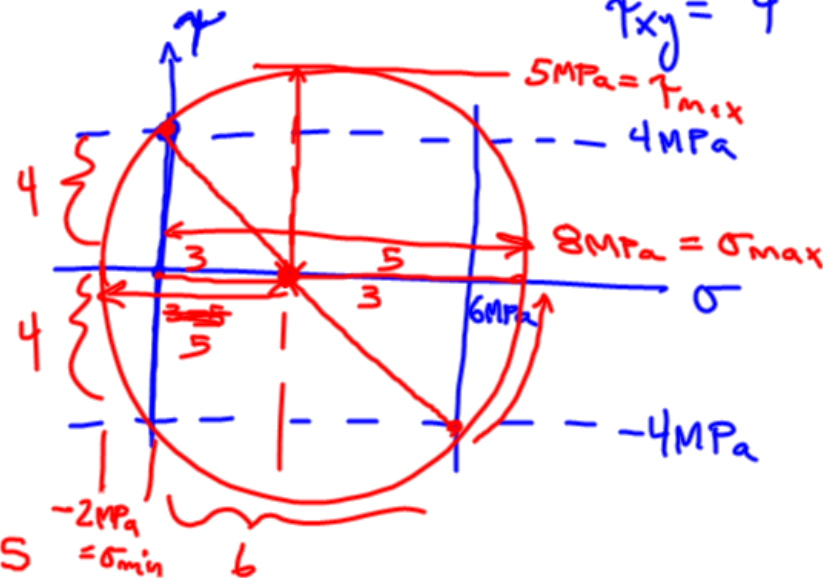
$$\sigma_{\max} = 8 \text{ MPa}$$

$$\sigma_{\min} = 3 - 5 = -2 \text{ MPa}$$

$$\sigma_x = 6$$

$$\sigma_y = 0$$

$$\tau_{xy} = 4$$



Determine the plane of normal stress in torsion.

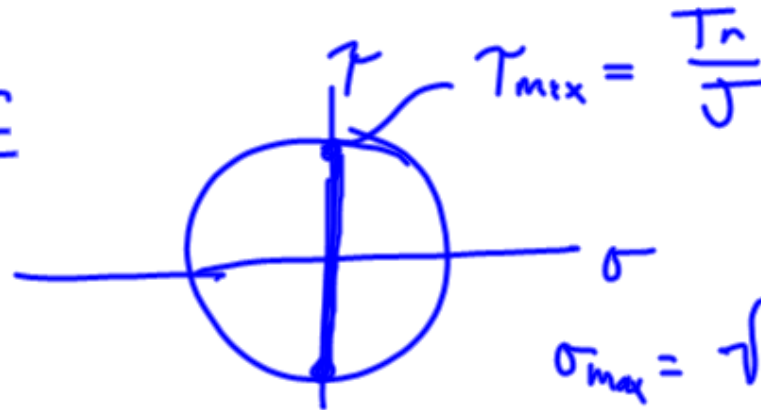


torsion only

$$\sigma_x = \frac{F}{A} = 0 \quad (\text{No axial force})$$

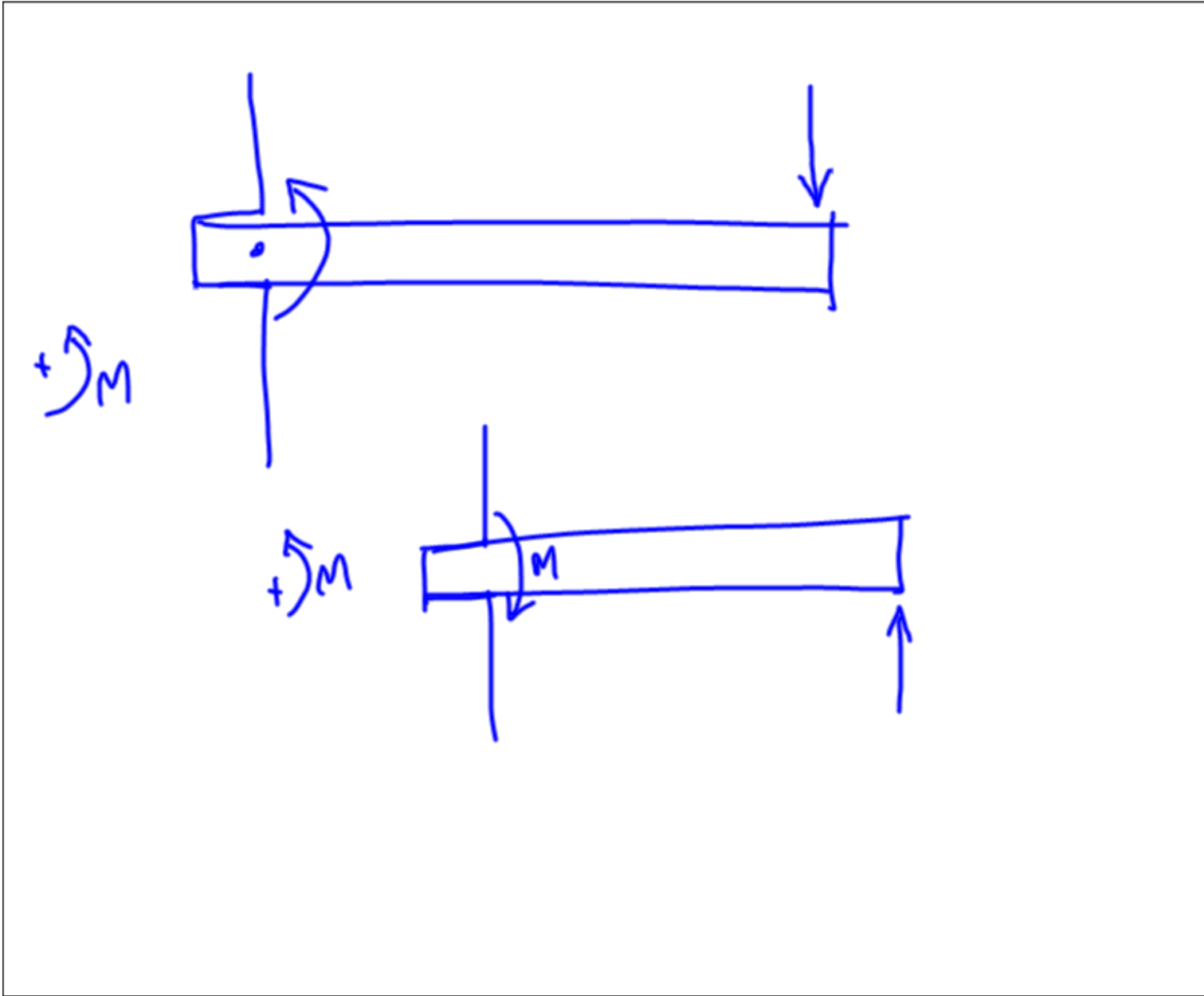
$$\sigma_y = \frac{M_z}{I_y} = 0 \quad (\text{No bending})$$

$$\tau_{xy} = \tau = \frac{T}{J} r$$



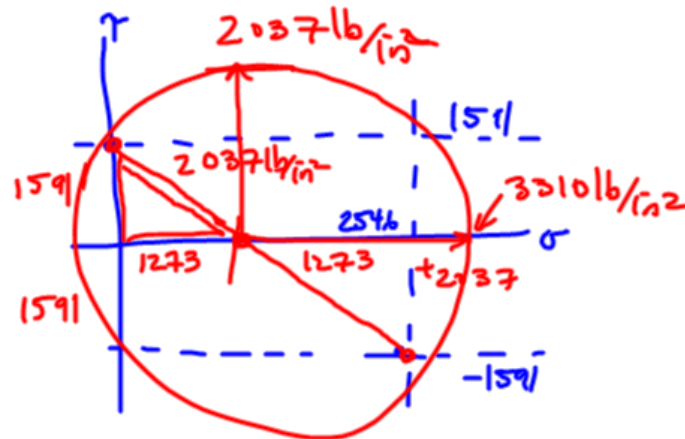
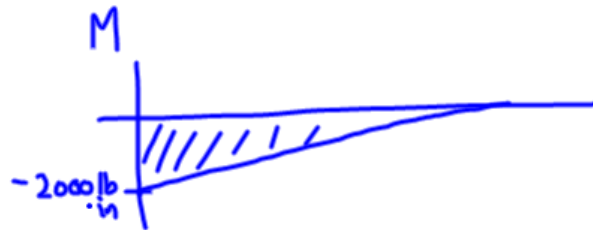
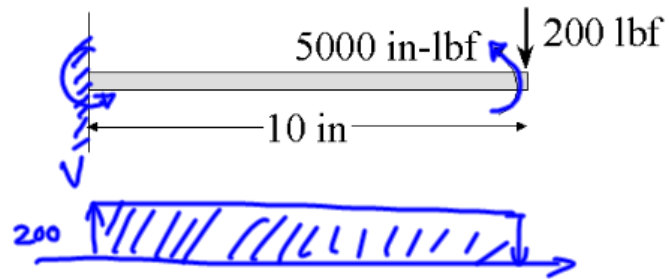
$$\sigma_{max} = \sqrt{\tau_{xy}^2}$$

$$\sigma_{min} = -\sqrt{\tau_{xy}^2}$$





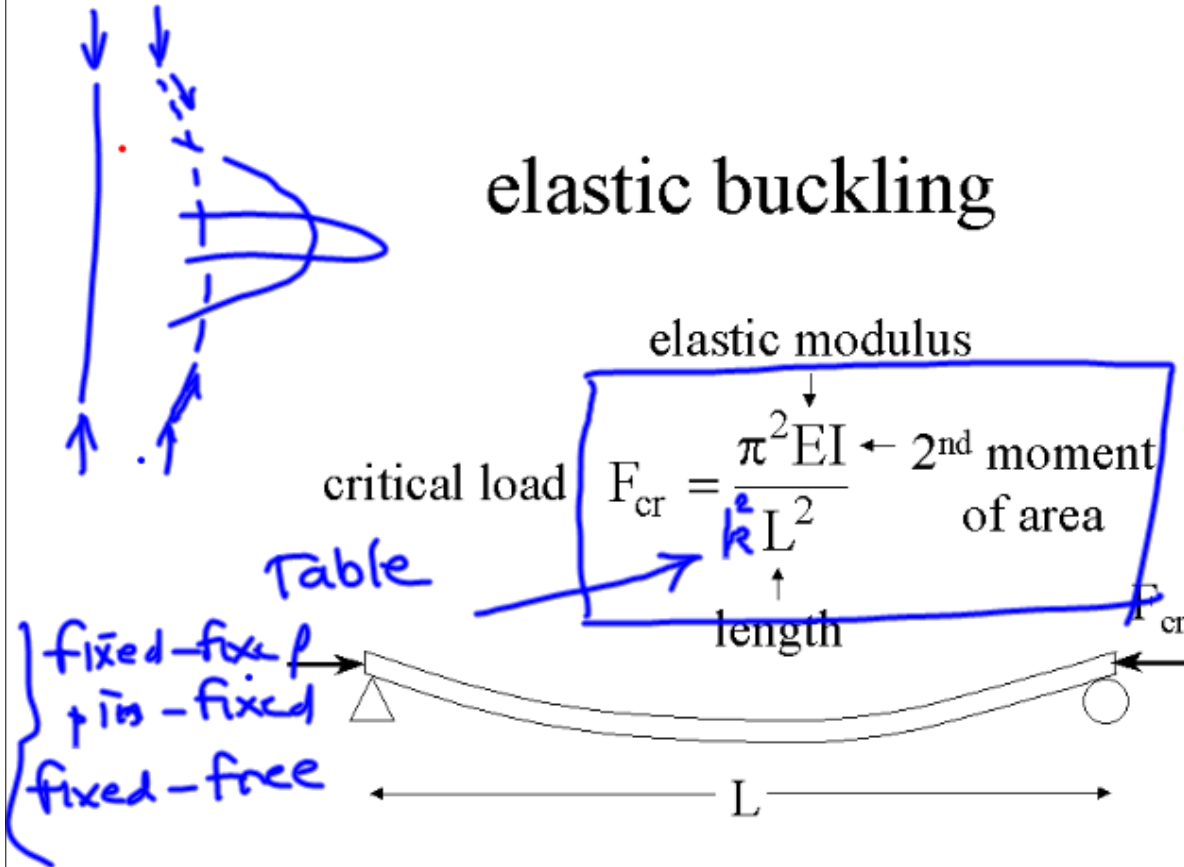
107. What is the maximum shearing stress at the fixed end of the 2 in. diameter shaft?



$$\begin{aligned} \sigma_x &= \frac{My}{I} \\ &= \frac{(2000 \text{ lb}\cdot\text{in})(1 \text{ in})}{\frac{\pi (1 \text{ in})^4}{4}} \\ &= \frac{4(2000)(1)}{\pi} \\ &= 2546 \frac{\text{lb}}{\text{in}^2} \end{aligned}$$

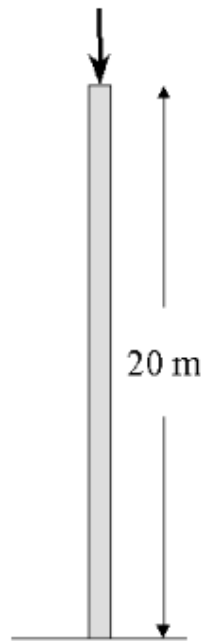
$$\begin{aligned} \tau &= \frac{T\rho}{J} \\ &= \frac{5000 \text{ lb}\cdot\text{in} (1 \text{ in})}{\frac{\pi (2 \text{ in})^2}{32}} \\ &= 1591 \frac{\text{lb}}{\text{in}^2} \end{aligned}$$

# elastic buckling



Use "2L" in place of "L" for a cantilever beam.

106. A 20 m flag pole is made of a 6 cm diameter steel ( $E = 210 \text{ GPa}$ ). What is the maximum axial load, using 2 as a factor of safety.



$$P_{cr} = \frac{\pi^2 EI}{k^2 L^2}$$

$$L = \frac{P_{cr}}{2}$$

$$\text{Load} = \frac{\pi^2 (210 \cdot 10^9 \text{ Pa}) (0.03^4 / 4) \pi}{2^2 \cdot (20 \text{ m})^2}$$

↑ "table"
fixed-free  
 $k=2$

$$= 412 \text{ N}$$