

**TEXAS TECH UNIVERSITY**  
**DEPARTMENT OF CIVIL, ENVIRONMENTAL, AND CONSTRUCTION ENGINEERING**

**Lab Report #7: Two-Stage Centrifugal Pump Characteristics**

**CE 3105 – Fluid Laboratory**

**Section**

**Team Number:**

**Instructor:**

**Authors:**

**Date of Experiment:**

**Date of Submission:**

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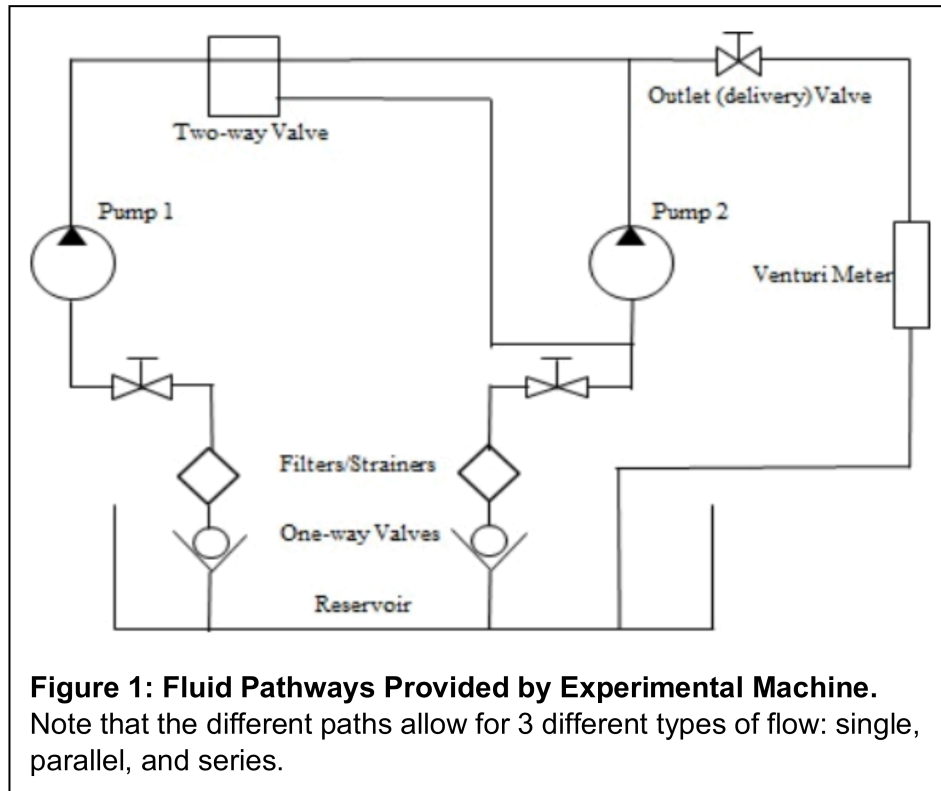
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## THEORY

For this experiment, we use a machine capable of sending water through a single line of flow, flow in parallel, and flow in series. Pressure readings at different points in the machine allow us to analyze changes across different types of flow. **Figure 1** shows the layout of the machine.



**Figure 1: Fluid Pathways Provided by Experimental Machine.**

Note that the different paths allow for 3 different types of flow: single, parallel, and series.

For single-line flow, the pressure drop across Pump 1 represents the total head. This is expressed as:

$$= P_{1(out)} - P_{1(in)} \quad (1)$$

For parallel flow, we must consider both pumps. The total head is given as:

$$= (P_{1(out)} + P_{2(out)}) - \frac{P_{1(in)} + P_{2(in)}}{2} \quad (2)$$

For flow in series, we again consider both pumps. The total head is found using:

$$= P_{2(out)} - P_{1(in)} \quad (3)$$

To find the total mechanical power of the input, we use:

$$W_1 = \frac{2\pi NT}{60} \quad (4)$$

$W_1$  = total mechanical input power of pump

$N$  = revolutions per minute (RPM) of pump

$T$  = torque

To find the hydraulic power of the pump:

$$W_2 = \quad (5)$$

$W_2 = \text{hydraulic power (horsepower) of pump}$

$H = \text{total head (varies based on flow pattern)}$

$Q = \text{flow rate (discharge)}$

To find the overall efficiency of the pump:

$$\eta = \frac{W_2}{W_1} \quad (6)$$

To find the flow rate:

$$Q = C_d A_1 \sqrt{\frac{2\Delta P}{\rho \left( \frac{A_1^2}{A_2^2} - 1 \right)}} \quad (7)$$

$Q = \text{flow rate (discharge)}$

$C_d = \text{coefficient of discharge (0.97)}$

$A_1 = \text{venturi inlet area}$

$\Delta P = \text{pressure drop}$

$\rho = \text{density of fluid}$

$A_2 = \text{venturi throat area}$

Using similarity laws and dimensionless analysis, we derive the following 4 equations:

**Table 1: Dimensionless Characteristics of Flow**

Solved parameter	Equation	#
Flow coefficient	$C_Q = \frac{Q}{N_r D^3}$	8
Head coefficient	$C_H = \frac{gH}{N_r^2 D^2}$	9
Power coefficient	$C_P = \frac{W_2}{\rho N_r^3 D^5}$	10
Reynold's number	$Re = \frac{\rho N_r D^2}{\mu}$	11

These are the concepts utilized during this experiment and its analysis.

## APPARATUS

### Figure 2: Two-Stage Centrifugal Pump System and Other Apparatuses used in Experiment

Depicted below is the experimental machine used to collect the data. Not depicted is a thermometer used to measure the temperature of the water.



### EXPERIMENT PARAMETERS

**1. Outlet Pressure & Inlet Pressure (lb/ft<sup>2</sup>)**

The difference between them is the total head.

**2. Discharge (ft<sup>3</sup>/s)**

This is the flow rate.

**3. Input Power & Output Power (ft --- lb/s)**

These were recorded from the machine used during the experiment.

**4. Coefficient of Discharge**

This is a given value. The coefficient of discharge is 0.97.

**5. Flow Coefficient, Head Coefficient, & Power Coefficient**

These can be calculated with equations from the theory portion of the report.

**6. Torque (lb\*ft)**

Torque can be found with the input power and an equation listed in the theory section.

**7. Density (slug/ft<sup>3</sup>)**

The density recorded of the water used in the experiment is based on the temperature being 20 degrees Celsius. The density of the water is 1.94 slugs per cubic foot.

**8. Pressure Drop (lb/ft<sup>2</sup>)**

This is the change in pressures calculated in the experiment.

**9. Efficiency**

This is the ratio between the output and input powers.

**10. Net Pressure (Pa)**

This is the pressure change across the pump.

**11. Impeller Diameter (ft)**

This is a given value. The impeller diameter is 0.37 feet.

## RESULTS

**Table 2: Two-Stage Centrifugal Pump Characteristics Collected data – Single Pump Test**

Below is the data table of recorded data from the single pump test. The parameters measured were pressure, pressure drop, torque, speed, and power.

P_2	P_3	P_4	$\Delta P$	Torq.	Pump 1 Speed (N_1)	W_1
-.41	.07	.17	.15	.74	3016	.5
-.30	.00	.00	.00	.00	3016	.01
-.22	.00	.00	.04	.55	3025	

**Table 3: Two-Stage Centrifugal Pump Characteristics Data Sheet – Series Pump Test**

Below is the data table of recorded data from the series pump test. The parameters measured were pressure, pressure drop, torque, speed, and power.

P2	P3	P4	$\Delta P$	Torq. (1)	Torq. (2)	Pump 1 Speed (N1)	Pump 2 Speed (N2)	W1 Pump 1	W2 Pump 2
-.40	.26	.21	.21	.78	.80	3007	3000	.247	.252
-.37	.22	.18	.22	.76	.76	3000	3004	.25	.240
-.32	.41	1.42	.11	.55	.55	3010	3010	.219	.219
-.24	.71	1.96	.06	.58	.60	3010	3010	.185	.18

**Table 4: Two-Stage Centrifugal Pump Characteristics Data Sheet – Parallel Pump Test**

Below is the data table of recorded data from the parallel pump test. The parameters measured were pressure, pressure drop, torque, speed, and power.

P2	P3	P4	$\Delta P$	Torq. (1)	Torq. (2)	Pump 1 Speed (N1)	Pump 2 Speed (N2)	W1 Pump1	W2 Pump2
-.21	-.51	.43	.42	.66	.61	30	30		
-.21	-.31	.93	.42	.66	.61	3010	3010	.170	.170
-.12	-.14	1.4	.03	.35	.31	3032	3024	.100	.100

**Table 5: Two-Stage Centrifugal Pump Characteristics Data Sheet - Calculations**

The data table below shows the calculated net pressures, discharges, output powers, and efficiencies of the five trials of each of the three tests.

Test Type	H	Q	W_2	$\Pi$
-----------	---	---	-----	-------

<b>Single Pump</b>	4 3000	.0 9	20	.92
	7 3000	.0 5	1 8	.51
	9 0000	.0 7	1 5	.70
	9 0000	.0 8	14 0	.80
	1 8000	.0 1	17 5	.90
<b>Series Pump</b>	7 000	.1 7	1 2	.40
	9 000	.1 2	2 5	.50
	12 000	.1 3	2 6	.70
	17 000	.0 5	3 9	.90
	22 000	.0 3	2 8	1.00
<b>Parallel Pump</b>	84 00	.1 8	2 5	.90
	94 00	.1 5	3 3	1.00
	119 00	.2 7	6 4	2.00
	140 00	.2 3	8 5	4.00
	153 00	.3 3	9 0	6.00

# DISCUSSION

## EXPERIMENT PURPOSE

The purpose of this experiment is to observe the performance of a single, series, and parallel connected pumps. From our results we obtained that series pumps had the advantage when it came to achieving a high net pressure(H). Parallel connection provided higher efficiency with a steadier discharge of the higher flow rates.

## REPORT QUESTIONS

1. For the Single Pump Test, explain the performance (relation between efficiency, head and flow rate). What do you think is the best efficiency?

From our results we can see that efficiency drops off when the flow rate increases. Flow rate also has an impact towards H and head coefficient. As flow rate decreases both H and the head coefficient increase. We believe that the best efficiency would be around the 80-90% range since the input power increases with a worse efficiency with a lower head coefficient.

2. Compare the performance of series and parallel pump tests against the single pump test.

Both the series and parallel connections tend to achieve a higher H compared to the series pump. The single pump provided slightly better efficiency compared to the series at the with their respective flow rate until they both ultimately achieved better efficiency. The parallel connection yielded a higher H, higher flow rate, and better efficiency to the single pump.

3. How does the total head curve change by parallel and series connections?

The difference in the total head curve between the two is what makes each connection unique. A series connection would have a summation of the heads depending on how many pumps are present. This would result in a much higher head. In a parallel connection the pumps connected would experience the same head in each. The total head curve would be much higher for a series connection compared to parallel.

4. How does the efficiency change by parallel and series connections?

In our results we found that the efficiency of the parallel connections was much higher compared to the series connection. Pumps in parallel are more efficient and provide a steady discharge while series instead in return provide a higher head.

5. Do the efficiencies of this experiment match with the typical large industrial pump efficiency (which is normally about 75%)? Why or why not?

We range of our efficiency varied but found with the curve that our most efficient percentage was close to the large industrial pump efficiency. From our single pump and series connection we saw the most efficient from the results was in the range between 80-90%. Our parallel connections exceeded the percentage. The efficiencies are close but do not match since this experiment was at a much smaller scale.

## PRACTICAL APPLICATION

This experiment observers the different behaviors between a single, series and parallel pump. In a practical application, to overcome a very long pipe with a high friction loss or a pipe set up

with a high static discharge head, the type of pump would be important. In the experiment we saw that the series pump had the advantage of producing a higher net pressure (H) than the parallel. In this case we would want to use pumps in series to successfully transport the fluid over the very long pipe or pipe with a high static discharge head.



## DATA APPENDIX

CE3105 Mechanics of Fluids Laboratory Department of Civil Engineering Texas Tech University

Experiment: Two Stage Centrifugal Pump Characteristics - Data Sheet

Date of Experiment: \_\_\_\_\_

Name: \_\_\_\_\_

Temperature of water,  $t =$  \_\_\_\_\_ °Celsius Water density,  $\rho =$  \_\_\_\_\_ (lb/ft<sup>3</sup>) Gravity,  $g = 32.2$  (ft/s<sup>2</sup>)

**Single Pump Test:**

P <sub>2</sub> (in.)	P <sub>3</sub>	P <sub>4</sub>	$\Delta P$	Torque (1) (in-lb)	Pump1 (N <sub>1</sub> ) (rpm)	W <sub>1</sub>	H (ft)	Q (ft <sup>3</sup> /s)	W <sub>2</sub> (ft/lb)	$\eta$
-.40	.07	.17	.15	.74	3010	235	58	.093	120.23	69%
-.35	.30	.43	.11	.72	3013	220	78	.085	138.49	85%
-.30	.47	.61	.09	.66	3016	210	90	.077	144.54	93%
-.28	.57	.71	.07	.63	3017	201	99	.068	140.22	94%
-.22	.80	.96	.04	.57	3027	177	118	.051	126.34	96%

**Series Pump Test:**

P <sub>2</sub>	P <sub>3</sub>	P <sub>4</sub>	$\Delta P$	Torque (1)	Torque (2)	Pump1 (N <sub>1</sub> )	Pump2 (N <sub>2</sub> )	Pump1 W <sub>1</sub>	Pump2 W <sub>2</sub>	H (ft)	Q (ft <sup>3</sup> /s)	W <sub>2</sub> (ft/lb)	$\eta$
-.49	-.26	.21	.21	.78	.80	2997	3000	247	252	70	.117	171.73	47%
-.46	-.13	.46	.19	.77	.79	2997	3002	242	247	92	.112	214.68	59%
-.44	.07	.40	.16	.75	.76	3000	3004	235	270	127	.103	265.53	76%
-.37	.41	1.42	.11	.68	.69	3006	3010	215	219	174	.085	308.99	96%
-.24	.71	1.96	.06	.58	.60	3015	3018	185	188	220	.063	288.49	105%

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Texas Tech University

Experiment: Two Stage Centrifugal Pump Characteristics - Data Sheet

Date of Experiment: \_\_\_\_\_ Name: \_\_\_\_\_

Parallel Pump Test:

P <sub>2</sub>	P <sub>3</sub>	Avg Inlet Press	P <sub>4</sub>	ΔP	Torque (1)	Torque (2)	Pump1 (N <sub>1</sub> )	Pump2 (N <sub>2</sub> )	Pump1 W <sub>1</sub>	Pump2 W <sub>2</sub>	H	Q	W <sub>2</sub>	η
-0.31	-0.51	-0.41	0.43	0.42	0.66	0.61	3005	3002	210	194	84	0.168	294.88	90 1/2
-0.21	-0.31	-0.25	1.22	0.10	0.44	0.39	3025	3011	124	140	140	0.283	824.86	125%
-0.15	-0.20	-0.13	1.4	0.03	0.35	0.31	3032	3024	112	100	153	0.303	969.13	618%
-0.12	-0.14	-0.13												

structor's Signature \_\_\_\_\_

Don Bundock

CE3105 Mechanics of Fluids Laboratory  
 Department of Civil Engineering  
 Texas Tech University

Experiment: Two-  
 Date of Experiment  
 Experimental D

team # Z

Temperature of water,  $T =$  celsius  
 Water density,  $\rho =$  ( $lb/ft^3$ )  
 Gravity,  $g = 32.2$  ( $ft/s^2$ )

Single pump Test:

$P_2$ bar	$P_3$ bar	$P_4$ bar	$\Delta P$ bar	Torque	Pump I Speed (rpm)	$W_1$	H kPa	Q	$W_2$	"
-0.41	0.07	0.17	0.15	0.74	3010 rpm	235	58	0.0993	120	0.1692
-0.35	0.30	0.43	0.11	0.73	3013 rpm	220	78	0.0950	138	0.851
-0.30	0.47	0.60	0.09	0.66	3016 rpm	210	90	0.0769	145	0.930
-0.18	0.57	0.71	0.07	0.63	3017 rpm	201	99	0.0678	140	0.943
-0.12	0.80	0.96	0.04	0.55	3024 rpm	177	118	0.0513	126	0.965

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Instructor's Signature



Series pump Test:

P <sub>2</sub>	P <sub>3</sub>	P <sub>1</sub>	ΔP	Torque (1)	Torque (2)	Pump 1 Speed (N <sub>1</sub> )	Pump 2 Speed (N <sub>2</sub> )	Pump 1 W <sub>1</sub>	Pump 2 W <sub>1</sub>	H (kPa)	Q	W <sub>2</sub>	η
-0.119	-0.710	0.21	0.21	0.78	0.80	<del>2997</del> 2997 rpm	3000 rpm	<del>247</del> 242	252	<del>92</del> 92	.117	172	0.4105
-0.140	-0.13	0.110	0.19	0.77	0.79	2997 rpm	3002 rpm	242	247	92	.112	215	0.5973
-0.110	0.07	0.84	0.10	0.75	0.70	3000 rpm	3004 rpm	235	240	124	.103	200	0.795
-0.32	0.41	1.42	0.11	0.08	0.09	3000 rpm	3010 rpm	215	219	174	.0850	309	0.902
-0.24	0.31	1.90	0.00	0.58	0.00	3015 rpm	3018 rpm	185	188	220	.0628	288	1.05

Parallel pump Test:

P <sub>2</sub>	P <sub>3</sub>	Avg. Inlet Pressure	P <sub>1</sub>	ΔP	Torque (1)	Torque (2)	Pump 1 Speed (N <sub>1</sub> )	Pump 2 Speed (N <sub>2</sub> )	Pump 1 W <sub>1</sub>	Pump 2 W <sub>1</sub>	H (kPa)	Q	W <sub>2</sub>	η
-0.31	0.51	-0.11	0.43	0.42	0.100	0.101	3005 rpm	3002 rpm	210	194	84	.108	295	.980
-0.28	-0.144	-0.20	0.58	0.30	0.03	0.58	3009 rpm	3005 rpm	300	185	94	.145	383	1.35
-0.21	-0.31	-0.20	0.93	0.21	0.53	0.49	3018 rpm	3011 rpm	170	150	119	.247	614	2.55
-0.15	-0.20	-0.195	1.22	0.10	0.44	0.39	3025 rpm	3019 rpm	138	124	140	.283	825	4.25
-0.12	-0.14	-0.13	1.40	0.03	0.35	0.31	3032 rpm	3024 rpm	112	100	153	.303	909	6.18

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Experiment: Two Stage Centrifugal Pump Characteristics - Data Sheet

Date of Experiment \_\_\_\_\_ Name: \_\_\_\_\_

Temperature of water, T= 20 °Celsius Water density,  $\rho$  = \_\_\_\_\_ (lb/ft<sup>3</sup>) Gravity, g= 32.2 (ft/s<sup>2</sup>)

Single Pump Test:

P <sub>2</sub>	P <sub>3</sub>	P <sub>4</sub>	$\Delta P$	Torque (1)	Pump1 (N <sub>1</sub> )	W <sub>1</sub>	H	Q	W <sub>2</sub>	$\eta$
<u>-.41</u>	<u>.07</u>	<u>.17</u>	<u>.15</u>	<u>.74</u>	<u>3010<sup>50</sup></u>	<u>235</u>				
<u>-.30</u>	<u>.47</u>	<u>.60</u>	<u>.07</u>	<u>.66</u>	<u>3017</u>	<u>210</u>				
<u>-.28</u>	<u>.57</u>	<u>.71</u>	<u>.07</u>	<u>.63</u>	<u>3017</u>	<u>201</u>				
<u>-.22</u>	<u>.80</u>	<u>.96</u>	<u>.04</u>	<u>.59</u>	<u>3025</u>	<u>177</u>				

Series Pump Test:

P <sub>2</sub>	P <sub>3</sub>	P <sub>4</sub>	$\Delta P$	Torque (1)	Torque (2)	Pump1 (N <sub>1</sub> )	Pump2 (N <sub>2</sub> )	Pump1 W <sub>1</sub>	Pump2 W <sub>2</sub>	H	Q	W <sub>2</sub>	$\eta$
<u>-.49</u>	<u>-.26</u>	<u>.21</u>	<u>.21</u>	<u>.78</u>	<u>.80</u>	<u>2997</u>	<u>3000</u>	<u>247</u>	<u>252</u>				
<u>-.46</u>	<u>-.13</u>	<u>.16</u>	<u>.19</u>	<u>.77</u>	<u>.79</u>	<u>2997</u>	<u>3000</u>	<u>247</u>	<u>247</u>				
<u>-.40</u>	<u>.01</u>	<u>.01</u>	<u>.10</u>	<u>.77</u>	<u>.77</u>				<u>240</u>				
<u>-.36</u>	<u>.41</u>	<u>1.42</u>	<u>.11</u>	<u>.68</u>	<u>.69</u>	<u>3006</u>	<u>3010</u>	<u>215</u>	<u>219</u>				
<u>-.24</u>	<u>.71</u>	<u>1.96</u>	<u>.06</u>	<u>.58</u>	<u>.60</u>	<u>3015</u>	<u>3019</u>	<u>195</u>	<u>188</u>				

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Experiment: Two Stage Centrifugal Pump Characteristics - Data Sheet

Date of Experiment: \_\_\_\_\_ Name \_\_\_\_\_

Parallel Pump Test:

P <sub>2</sub>	P <sub>3</sub>	Avg Inlet Press	P <sub>4</sub>	Δ P	Torque (1)	Torque (2)	Pump1 (N <sub>1</sub> )	Pump2 (N <sub>2</sub> )	Pump1 W <sub>1</sub>	Pump2 W <sub>2</sub>	H	Q	W <sub>2</sub>	η
-.3			.43	.42	.66	.61	3005	3002	210	174				
-.28	-.44						3009	3005	200	185				
-.21	-.31		.93	.21	.53	.79			170	156				
-.15	-.20		1.22	.10	.44	.39	3025	3012						
-.12	-.19		1.4	.03	.35	.31	3032	3024	112	100				

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_



## ERROR CALCULATIONS

There are not many sources of error that arise in this experiment since most of our calculations are taken from readings of the indicators on the apparatus. Some of the bar values fluctuated to a range of  $\pm .03$ .

In our results we also obtained extremely high efficiencies for the parallel connections. We were unable to determine if this error is correct or not, but the calculations follow.

$$\eta = \frac{W_2}{W_1} \text{ and } W_2 = (H) \cdot Q \rightarrow W_2 = \frac{(153000)(.303)}{100000} \cdot 2088.54 = 969.13 \text{ ft} \cdot \frac{\text{lb}}{\text{s}}$$

$$\text{Then } \eta = \frac{(969.13)}{(156.88)} \cdot 100 = 618\%$$

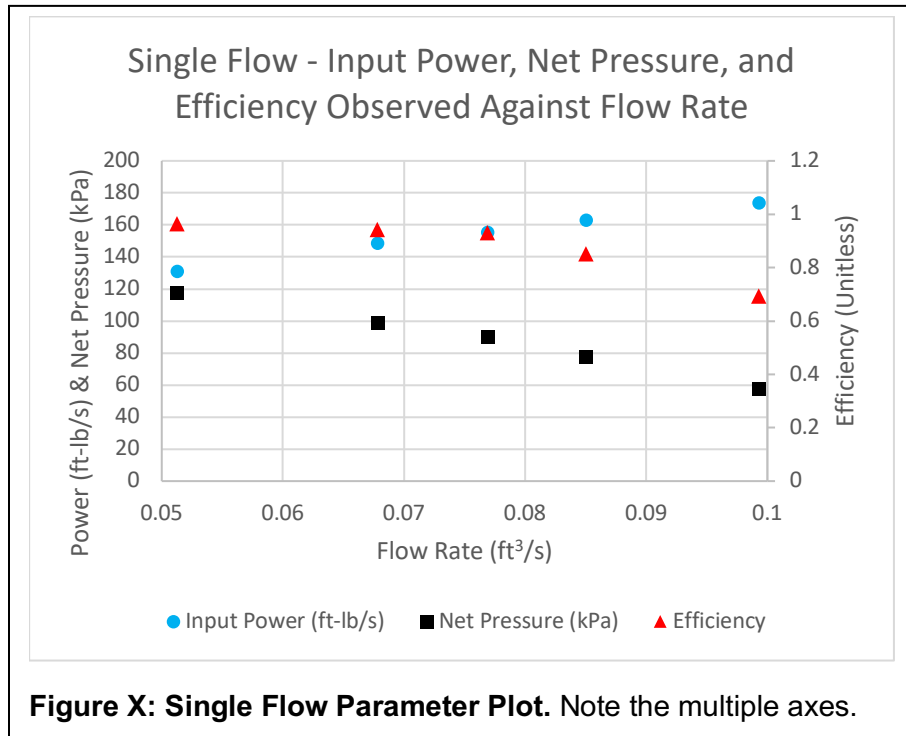
We also received very high values when calculating Reynolds number for the single pump. Sample calculation for the possible error.

$$Re = \frac{(\rho N_r D^2)}{\mu} = \frac{(1.9368 \cdot 315.94 \cdot .37^2)}{2.09e - 5} = 4009126.7$$

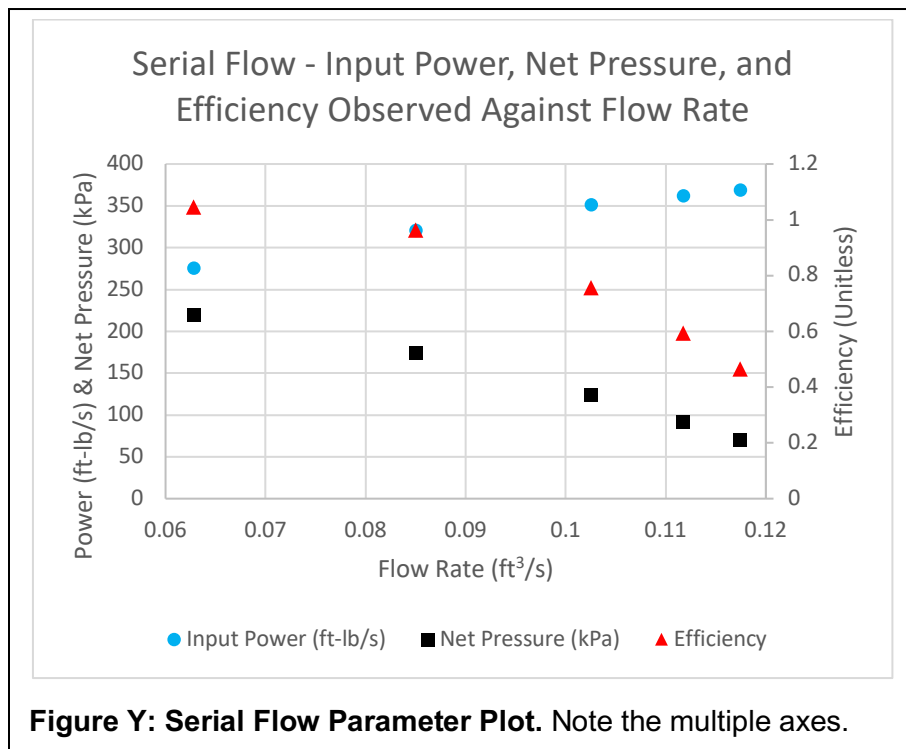
Each Re number ended up having a very high number similar to trial 4 shown above. We also know that the efficiency should not surpass 100 but ended up with values over at the last trial for series and many for parallel.

# SAMPLE CALCULATIONS

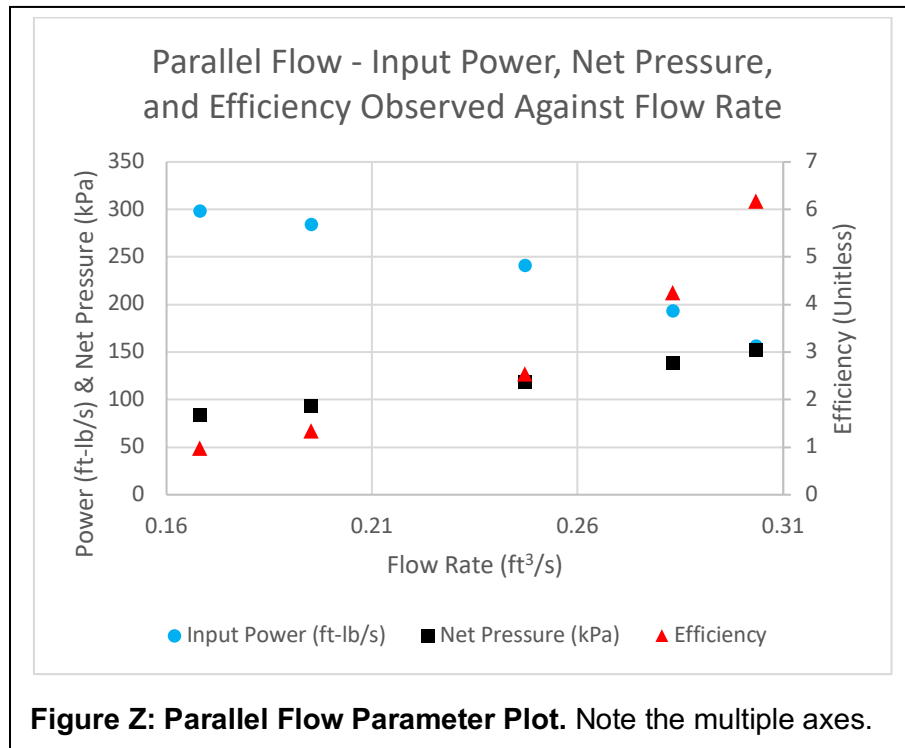
## SINGLE FLOW PLOT



## PARALLEL FLOW PLOT



### FLOW IN SERIES PLOT



#### HEAD LOSS – SINGLE FLOW

Using the formula given in the Calculations portion of the lab handout:

$$H = (P_4 - P_2) * (100000 \text{ Pa}/\text{bar})$$

We plug in values from Trial 1 of the single flow arrangement to obtain:

$$H = (0.17 \text{ bar} - (-0.041 \text{ bar})) * (100000 \text{ Pa}/\text{bar})$$

$$H = 21.1 \text{ kPa}$$

#### HEAD LOSS – SERIES FLOW

Using the formula given in the Calculations portion of the lab handout:

$$H = (P_4 - P_2) * (100000 \text{ Pa}/\text{bar})$$

We plug in values from Trial 1 of the serial flow arrangement to obtain:

$$H = (0.21 \text{ bar} - (-0.49 \text{ bar})) * (100000 \text{ Pa}/\text{bar})$$

$$H = 70.0 \text{ kPa}$$

**HEAD LOSS – PARALLEL PUMP**

Using the formula given in the Calculations portion of the lab handout:

$$H = \left( P_4 - \frac{P_2 + P_3}{2} \right) * (100000 \text{ Pa}/\text{bar})$$

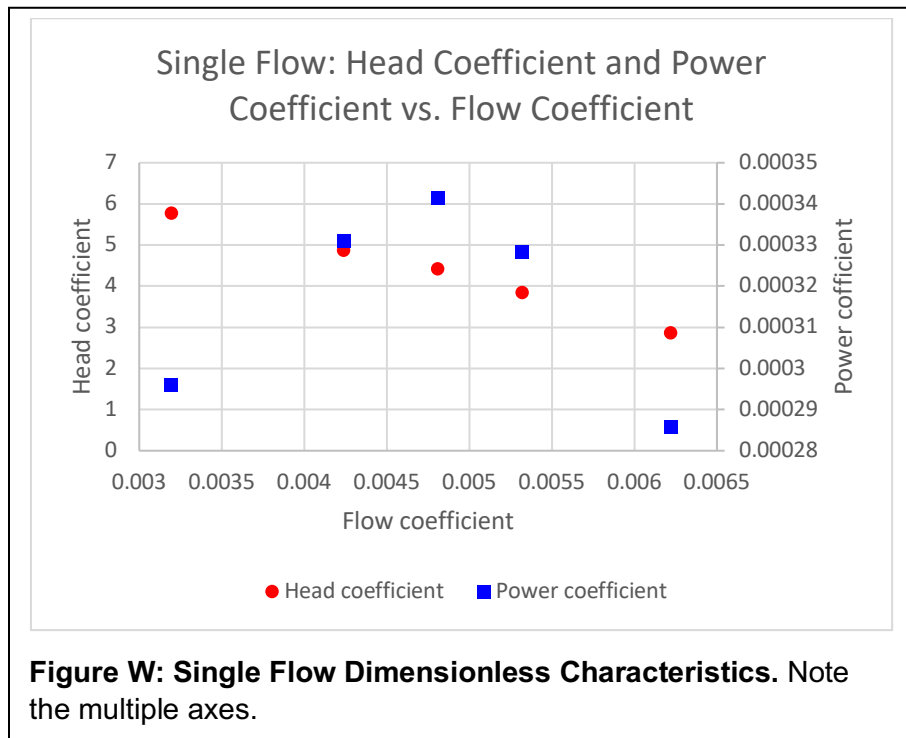
We plug in values from Trial 1 of the parallel flow arrangement to obtain:

$$H = \left( 0.43 \text{ bar} - \frac{-0.31 \text{ bar} + (-0.51 \text{ bar})}{2} \right) * (100000 \text{ Pa}/\text{bar})$$

$$H = 84.0 \text{ kPa}$$

**DIMENSIONLESS CHARACTERISTICS: SINGLE FLOW**

PLOT



**REYNOLD'S NUMBER**

Despite being checked, double-checked, and triple-checked, these Reynold's numbers ended up being ridiculously high. **Table [INSERT NUMBER HERE!!!]** shows the Reynold's numbers from the various trials. Despite being very high, they are all virtually the same, which is a good sign.

**Table 6: Reynold's Numbers for Single Flow Trials**

Trial #	1	2	3	4	5
Re	3999824.74	4003811.28	4007797.81	4009126.66	4019757.42